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THERMAL CHARACTERIZATION OF IRON OXIDE AND ALUMINUM OXIDE POWDERS BY EMANATION TflERMAL ANALYSIS

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ABSTRACT

Emanation thermal analysis (ETA) using a surface impregnation method of Ra-226 nuclide was applied for the thermal characterization of iron oxide and aluminum oxide powders with various preparation histories in the heating and grinding treatments.

INTRODUCTION

The role of the surface on the reactivity of powder increases with a decrease in particle size. The author has already reported on the applications of emanation thermal analysis (ETA) for the initial reactivity of metal oxide powders [1,2]. Further, the thermal characterization of iron oxide powders by ETA was reported [3].

In this paper, ETA using a surface impregnation method of Ra-226 nuclide was applied for the characterization of near-surface of iron oxide and aluminum oxide powders with various preparation histories in the heating and grinding treatments.

EXPERINENTAL

The apparatus used for ETA is commercially available Netzsch device (ETA 403 - STA 409) for simultaneous ETA-TG-DTA measurements. The standard experimental conditions were as follows; sample weight of 100mg, N_2 carrier gas of 50ml/min, heating rate of 10 $^{\circ}$ C/min, threshold of ZMeV, time constant of 300sec. The samples were labeled by a surface-impregnation method using $Ra-226$ solution $(4\mu C_1/ml)$ and dried without further washing the surface of labeled powders. Before being used for ETA experiments, in both first and repeated runs, the dried labeled-samples were stored respectively for the periods exceeding one month until a radioactive equilibrium state was reached.

Reagent grade commercial α -Fe₂O₃ (Kanto) and activated alumina (merck) were used as the starting materials. The ETA samples with various preparation histories are shown in Table 1. As an example, the sample No. F24 was prepared as follows; first the $Fe₂O₃$ powder (F2) compacted as a tablet was heated at 1300°C for 20hr in air,

then it was ground and sieved to obtaine a sive fraction between 100 and 150 mesh.

TABLE 1

Preparation methods of samples.

C': calcining in dispersed powders, rapid heating and cooling in air. G: G': grinding with a pestle, and sieving. grinding in acetone by ball-mill, and sieving.

m: mesh.

RESULTS AND DISCUSSION

When a state of radioactive equilibrium was reached in the dry labeled sample, Rn-222 gas is distributed in the surface layer smaller than 100nm thick [4]. On the basis of Balek's considerations [5], the radon release was grouped into three parts; (a) recoil part, E_r , due to the energy that radon atom gains during its formation by decay of radium, (b) a diffusion part, E_p , due to the diffusion in intergranular space, open pores, etc. of the dispersed powder and (c) a diffusion part, E_{d} , due to the bulk diffusion of radon in solid matrix of the dispersed powder. E_r is temperature-independent. E_n is dependent on temperature, and on dispersity or morpho'logy of the powders. E_A is dependent on temperature. A gas release for E_A -part starts between 40 and 50% of the melting temperature, $T_m(K)$, for a large variety of ionic crystals of different lattice structures [6]. The onset temperature of gas release for E_d -part is also similar to that of self-diffusion of matrix atoms. The characteristic changes in ETA curves obtained were observed in the following two stages; stage I due to E_p at temperature lower than $(0.4-0.5)T_m$, and stage II due to E_d at temperature higher than $(0.4-0.5)T_m$. The ETA peaks corresponding to the stages I and II are hereinafter represented by

Fig. 2(A, B). ETA curves for $Fe₂O₃$ powders (F22, F23, F24, F25) of different particle sizes with heating and grinding treatments.

 (A)

A11

 $df/dt') /$ cpm 200cpm (B) $_{II}$ AI I $\frac{800}{t/^{\circ}C}$ 1200 1600 400 0

 Π

Fig. 3. (A), ETA-DTA curves for activatedalumina (A10), and (B), its stepwise tests.

Fig. 4. (A), ETA curves for α -Al₂O₃ (All), and (B), its stepwise tests.

peaks I and II, respectively. The peak which appears at the temperature of about $(0.4-0.5)T_m$ was represented as peak I', because in the repeated run this peak shows a behavior similar to peak I. The temperature range of $(0.4-0.5)T_m$ is calculated as 456 - 639°C for α -Fe₂O₃ (T_m=1823K) and 656 - 889^oC for α -A1₂O₃ (T_m=2323K).

Figs. 1 and 2 show the ETA curves for various $I \circ 0_{7}$ powders (F21 - F25). The curves obtalned in first and repeated runs are represented by solid and dashed lines, respectively. The curves in first run greatly vary with the preparation history of sample, but in repeated run the curves lead to a single curve which has onset temperature of about 600°C and peak temperature of about 1OOO'C with a good reproducibility (see third run in Fig.1). Fig. 2 shows that in the first run peak I appears newly at 200 - 3OO'C as a result of a mechanochemica1 effects which were caused by the grinding treatment of the preheated samples, and peak II at about 9OO'C (Fig.1) shifts to a higher temperature side (1000°C) as a result of an ordering effect of crystal lattice by the heating treatments. For peak I' at about 600°C, however, it 1s thought-that both mechanochemical and ordering effects appear simultaneously at this temperature. These peaks I and 1' drsappear in the repeated run by the heating treatment.

Figs. 3 and 4 show the curves for activated alumina and α -Al₂O₃, respectively. In general, the results show a behavior similar to that of Fe₂O₃ powders. For activated alumina (A10) in Fig. 3, peak II initiates at about 800°C with peak temperature of about 127O'C corresponding to the transition to α -A1₂0₃ (see DTA curve). The ETA peak at about 300°C corresponds to the dehydration. In the repeated run, the curve leads to that of α -A1₂O₃ with peak II at 1350°C. In the stepwise tests shown in Fig. 4(B), the peaks I and I' disappear successively, finally lead to a single peak II at 1350°C.

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